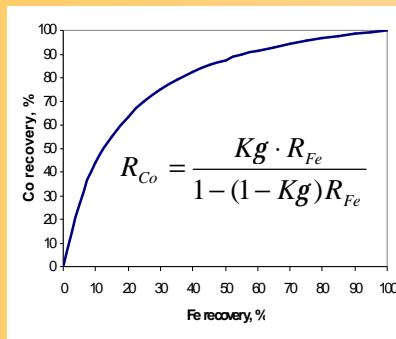


# Recovery of base metals and PGMs in a DC alloy-smelting furnace

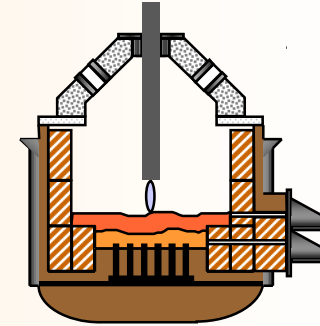


RT Jones  
IJ Geldenhuys  
QG Reynolds



## Introduction

- Reductive alloy smelting using carbon as a reducing agent:
  - Chromite smelting
  - Nickel laterite smelting
  - Recovery of base metals from slags
  - Collection of PGMs in iron alloys
- Amount of alloy increases with carbon addition
- Recovery of valuable metals is related to the recovery of iron



## Equilibrium description



$$K = \frac{a_{\text{Co}} \cdot a_{\text{FeO}}}{a_{\text{CoO}} \cdot a_{\text{Fe}}} \quad [1]$$

$$K = \frac{g_{\text{Co}} x_{\text{Co}} \cdot g_{\text{FeO}} x_{\text{FeO}}}{g_{\text{CoO}} x_{\text{CoO}} \cdot g_{\text{Fe}} x_{\text{Fe}}} \quad [2]$$

$$Kg = \frac{n_{\text{Co}} \cdot n_{\text{FeO}}}{n_{\text{CoO}} \cdot n_{\text{Fe}}} \quad [3]$$

## Mass balance equations

$$n_{Co} = n_{Co}^0 + n_{CoO}^0 - n_{CoO} \quad [4]$$

$$n_{Fe} = n_{Fe}^0 + n_{FeO}^0 - n_{FeO} \quad [5]$$

## Definition of recovery

$$R_{Co} \equiv \frac{n_{Co}}{n_{Co}^0 + n_{CoO}^0} \quad [6]$$

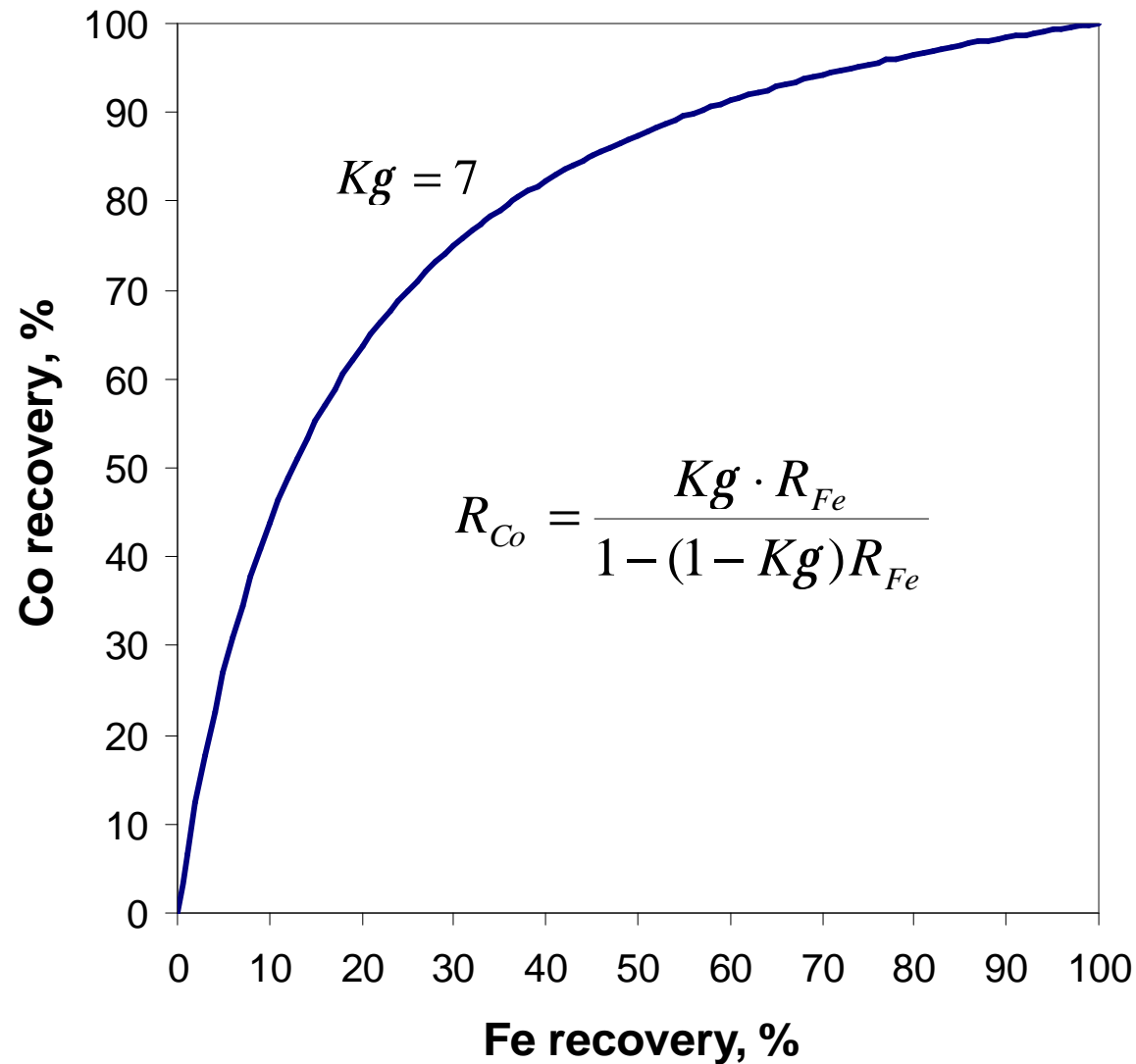
$$R_{Fe} \equiv \frac{n_{Fe}}{n_{Fe}^0 + n_{FeO}^0} \quad [7]$$

## *K<sub>g</sub>* Recovery Equation

$$K_g = \frac{R_{Co} (1 - R_{Fe})}{R_{Fe} (1 - R_{Co})} \quad [8]$$

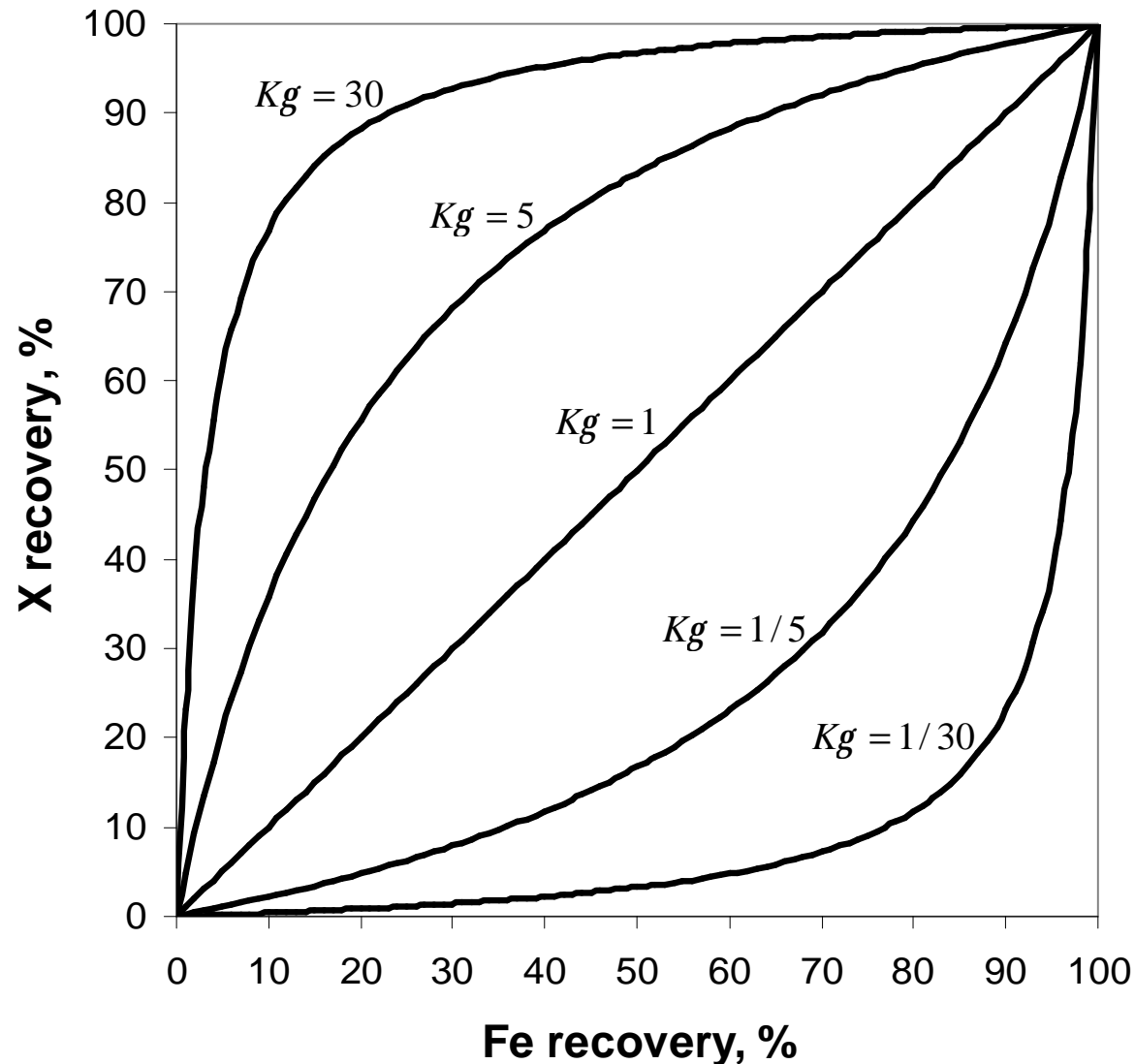
$$R_{Co} = \frac{K_g \cdot R_{Fe}}{1 - (1 - K_g) R_{Fe}}$$

## Co versus Fe Recovery



- $Kg$  can be calculated from equilibrium constant and activity coefficients, or fitted empirically

## Shape of recovery curve, and values of $K_g$



$$R_{Co} = \frac{K_g \cdot R_{Fe}}{1 - (1 - K_g)R_{Fe}}$$

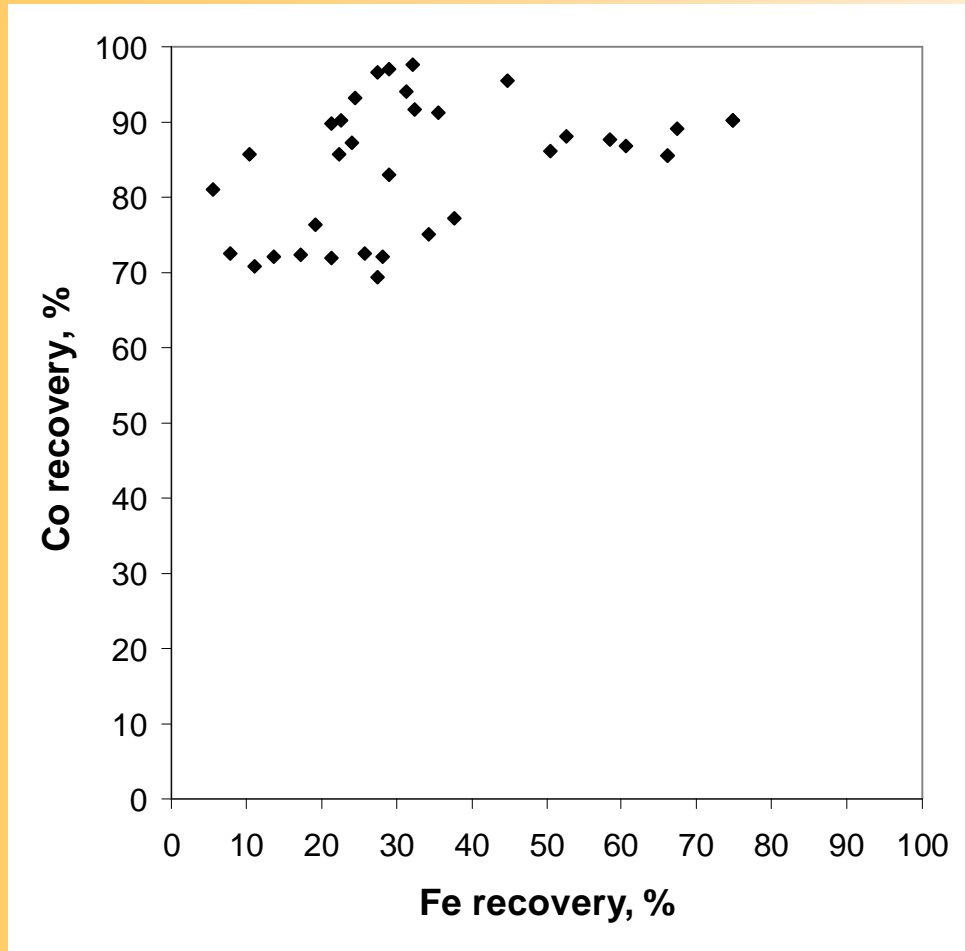
- $K_g = 1$  represents Fe
- Most 'noble' at top left

## Application to cobalt recovery from slag



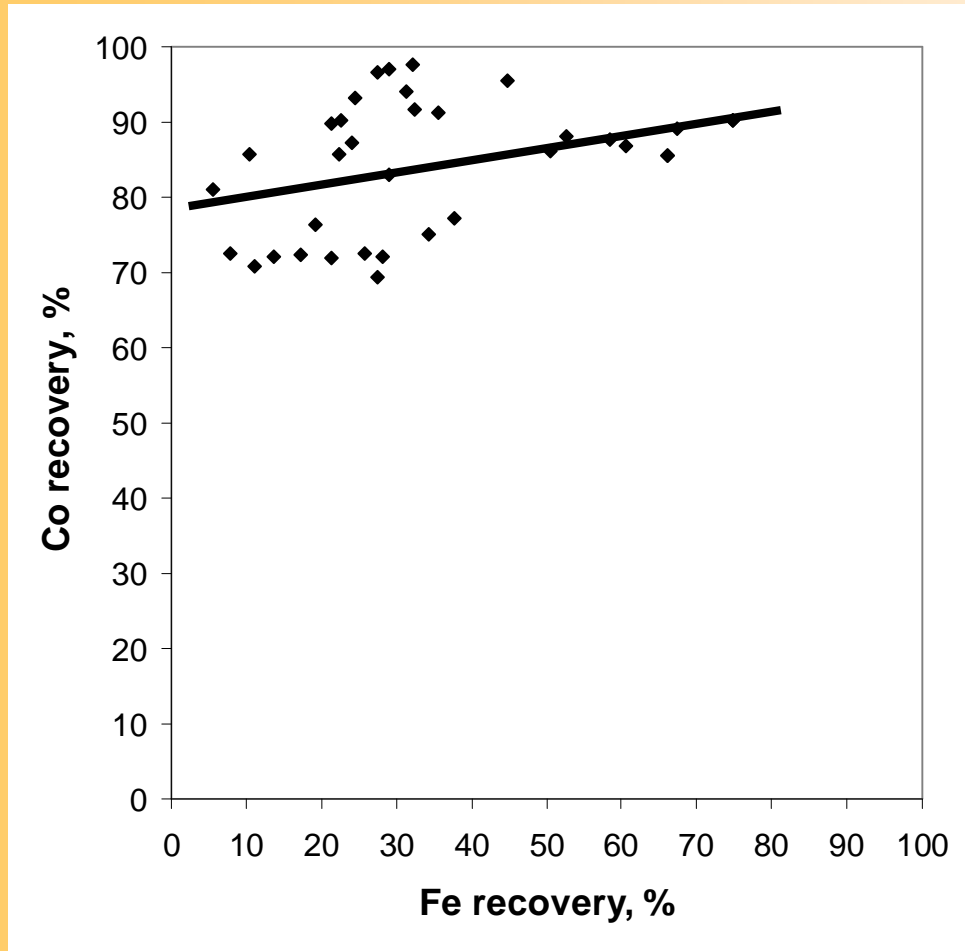
- Cobalt present as  $\text{CoO}$  in slag
- Need more than settling
- Oxides reduced by Fe, forming  $\text{FeO}$
- Carbonaceous reductant
- Temperature between 1500 and  $1600^{\circ}\text{C}$
- Aim to selectively reduce Co in preference to Fe

## Recovery of cobalt from copper reverberatory furnace slag



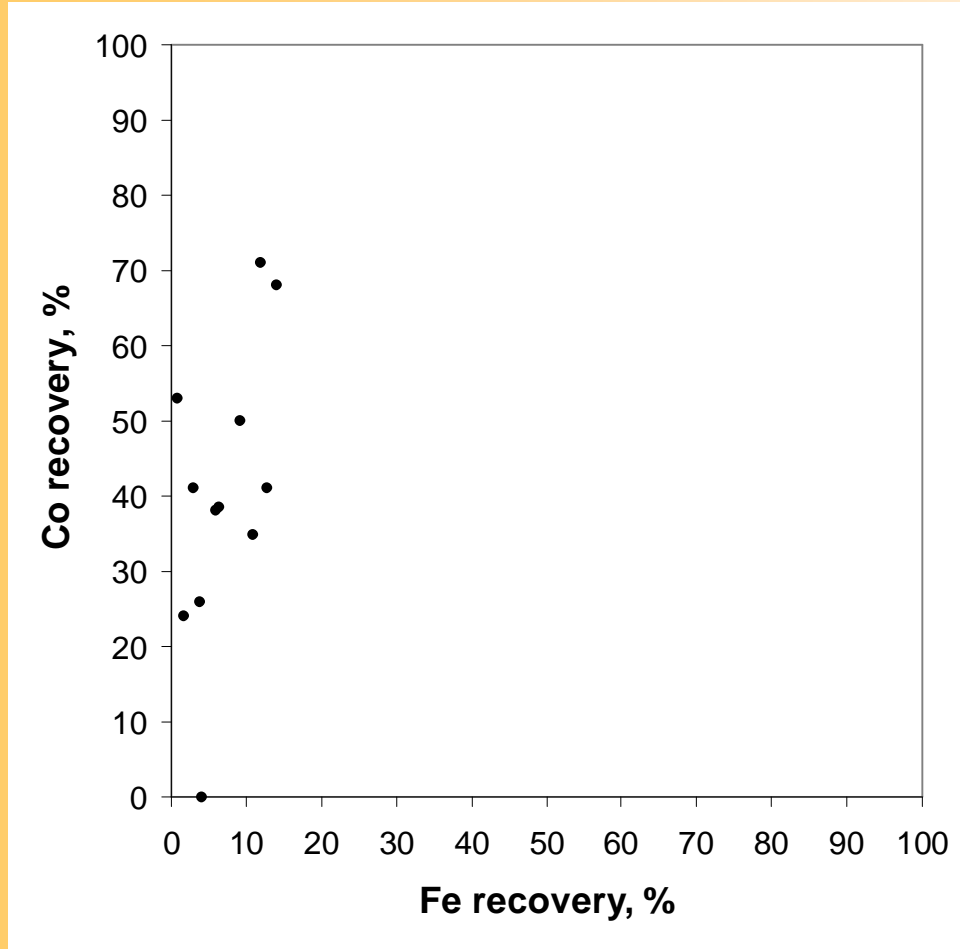
- A fair degree of scatter
- Wide range of experimental conditions
- Analytical uncertainties

## Recovery of cobalt from copper reverberatory furnace slag



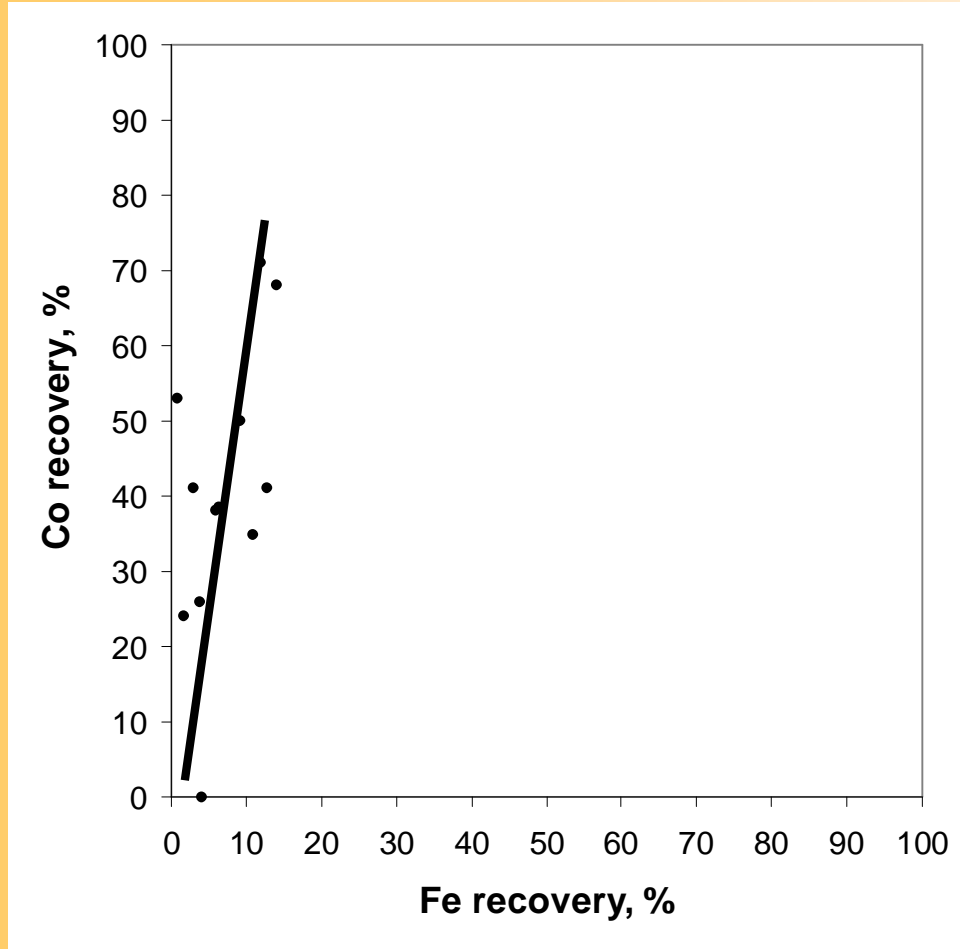
- Perhaps a straight line?

## Recovery of cobalt from flash furnace slag



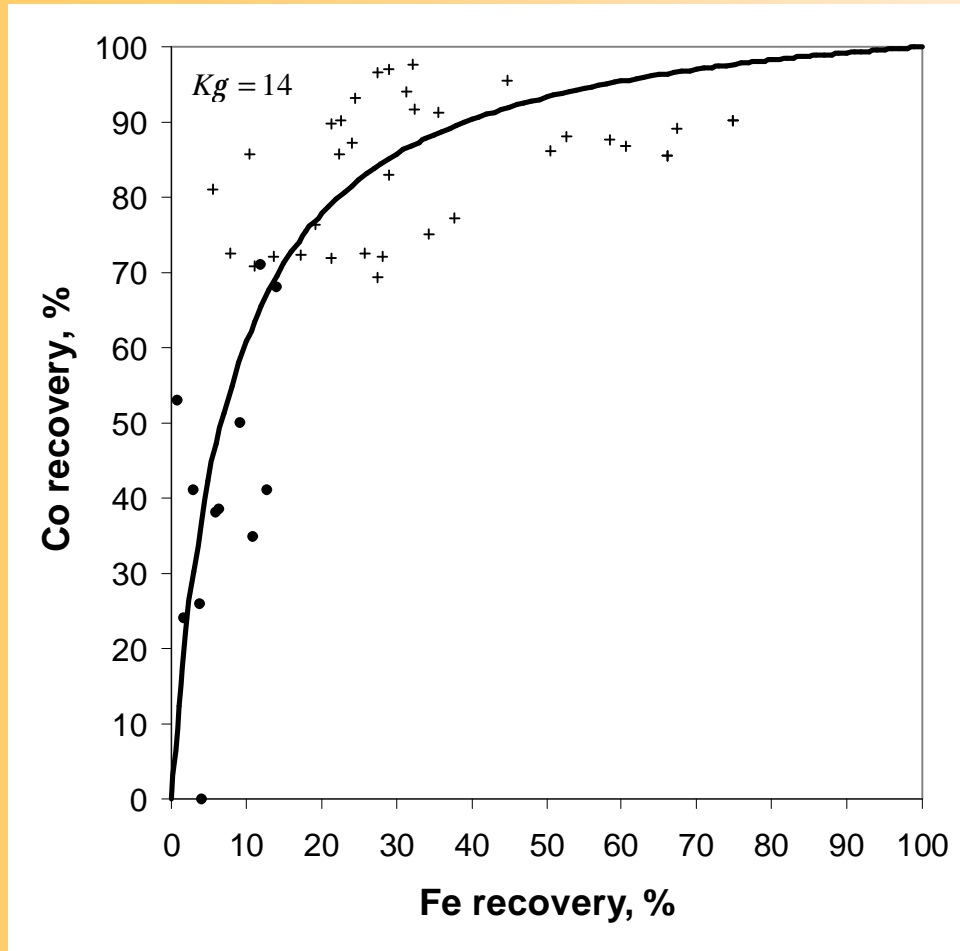
- Set of data with only small amounts of reduction
- Low recoveries

## Recovery of cobalt from flash furnace slag



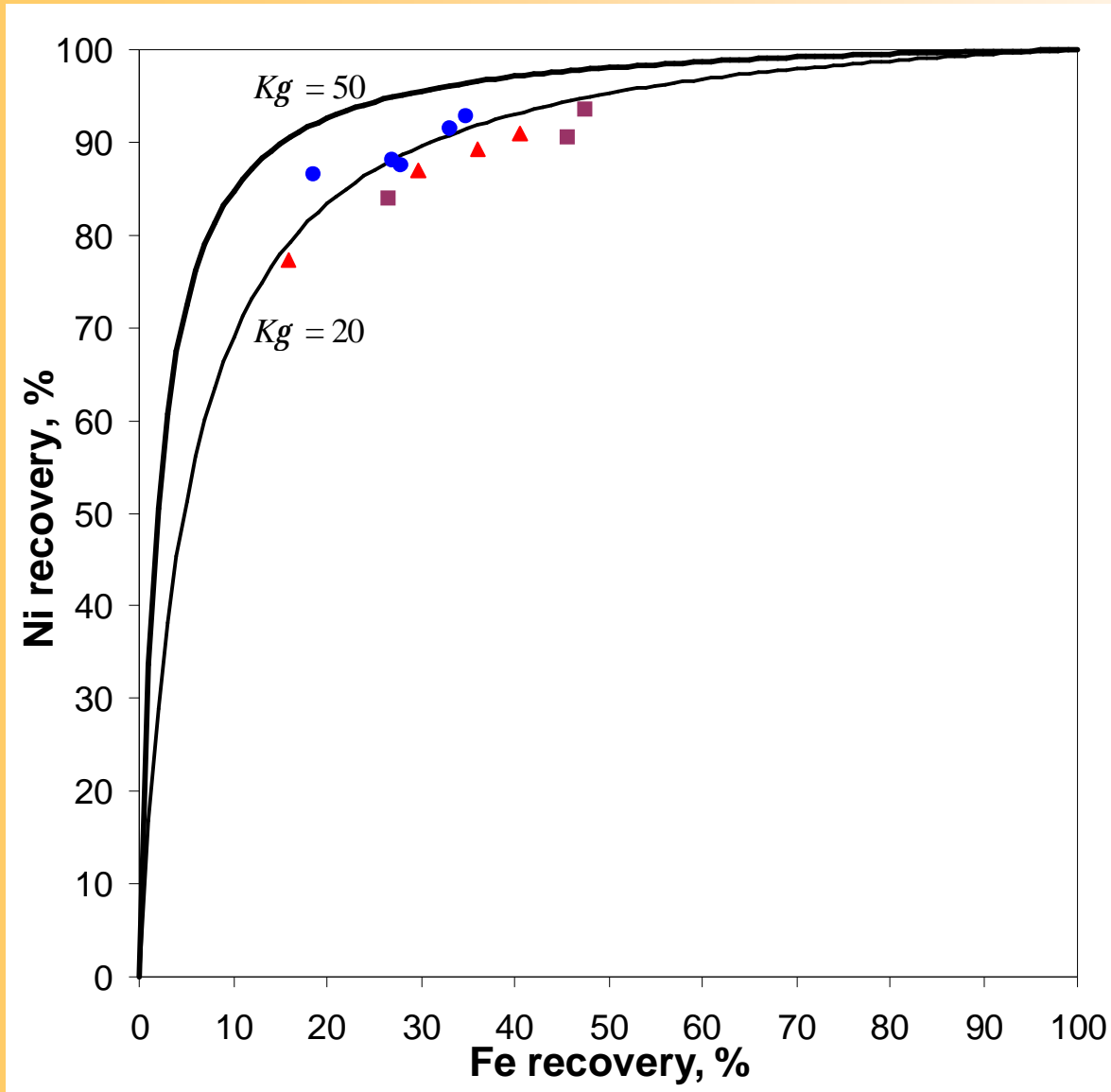
- Set of data with only small amounts of reduction
- Low recoveries
- Perhaps another straight line?

## Cobalt recovery from slag



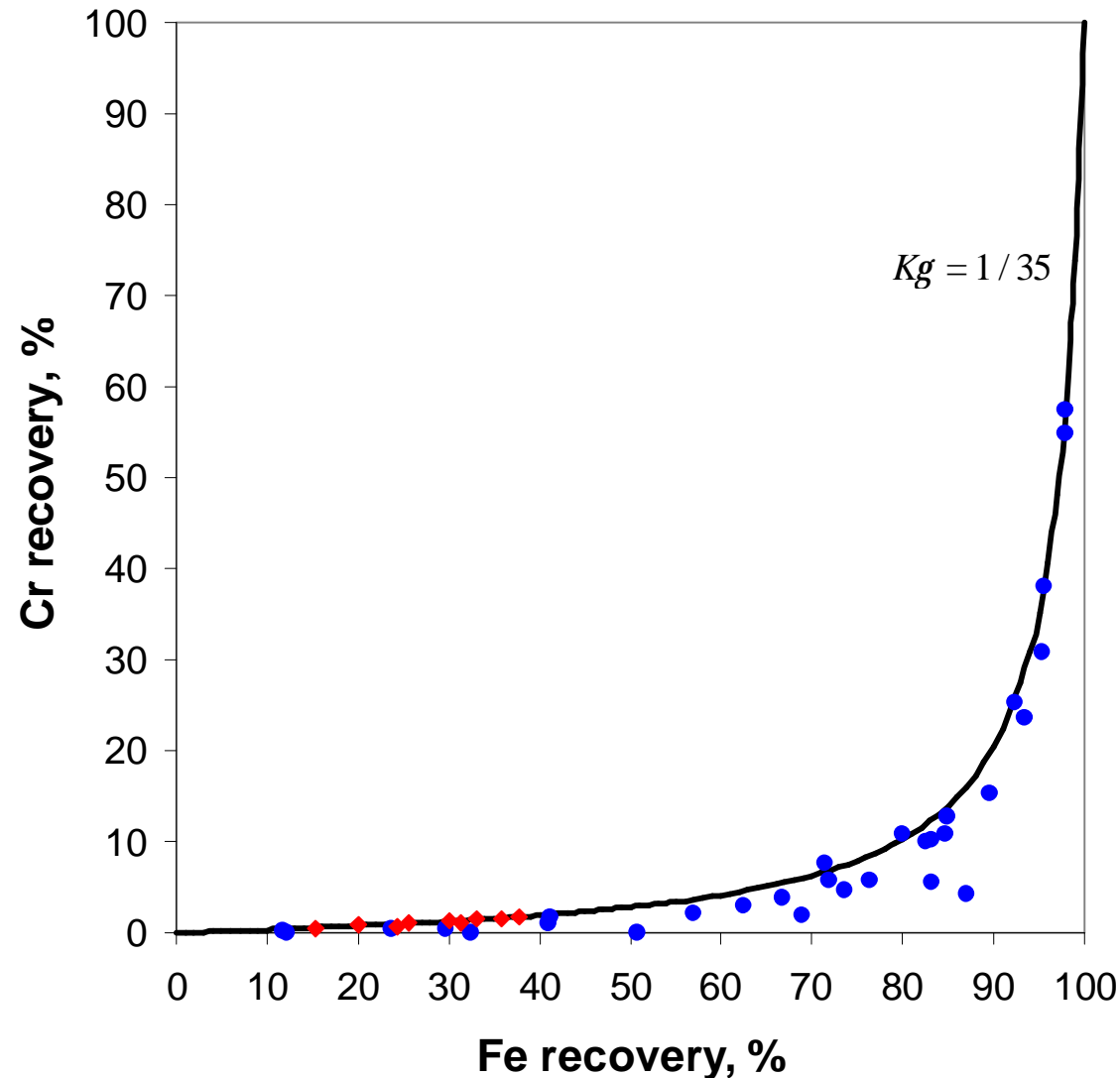
- The  $Kg$  recovery equation covers both ranges well
- $K = 30$
- $Kg = 13$  by theory
- $Kg = 14$  by fitting

## Application to ferronickel



- Ni follows the same pattern
- Data shown for three samples under different conditions, not necessarily at equilibrium
- Selection of  $Kg$ , 20 or 50?

## Cr in FeNi



- Cr recovery is usually very low in FeNi
- Lab tests can easily be over-reduced to make sufficient metal
- Excellent agreement with other (revert tailings) work too



## ConRoast PGM smelting

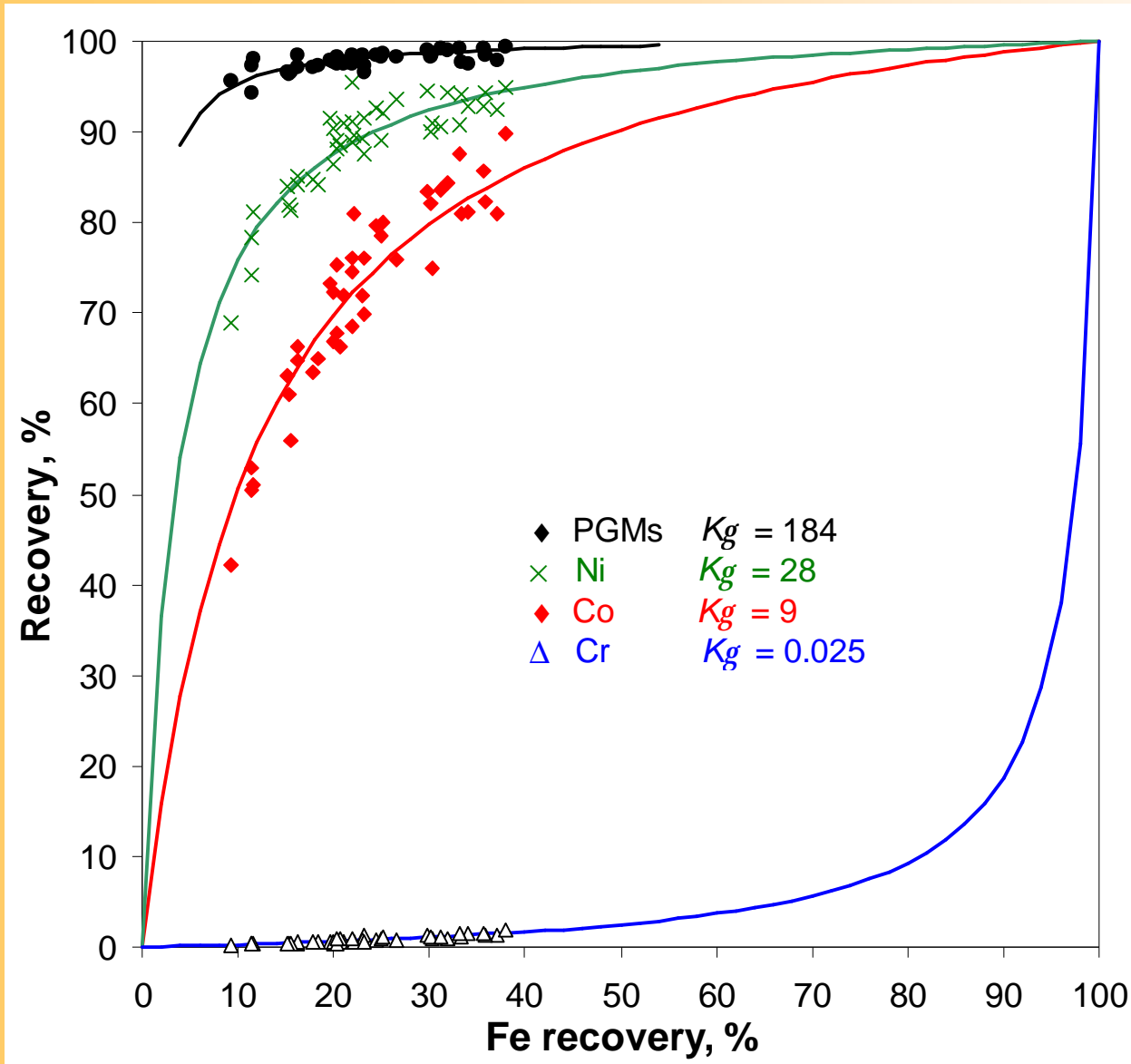
- ConRoast involves smelting low-S concentrates in a DC arc furnace and collecting valuable metals in an iron alloy
- Mintek operates a 3MW furnace that is designed to smelt up to 2000 tons per month

## PGM smelting

- 1.5 MW furnace
- 37 000 tons smelted over four years
- Each monthly data point represents hundreds of kg



## PGM smelting

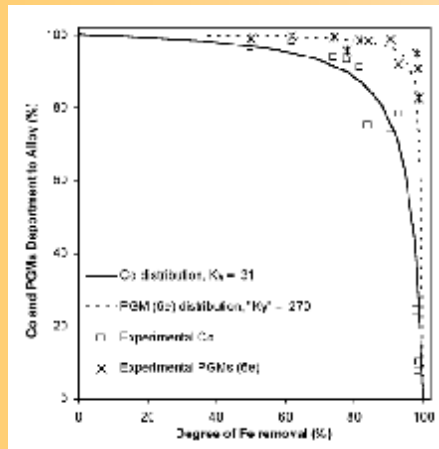


- Good reasons for using  $K_g$  on NiO, CoO, and CrO
- PGM behaviour can be modelled this way too (empirically)

## Application to oxidative converting processes

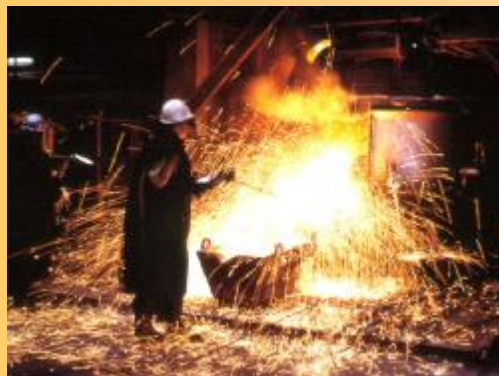


- Reductive smelting and oxidative converting are governed by the same chemical reactions (one is the reverse of the other)
- Recovery is plotted against degree of iron removal



# Mintek's DC furnaces

<http://www.mintek.co.za/Pyromet/>



# Mintek

